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**Automated sequential injection-capillary electrophoresis for dried blood spot analysis: A proof-of-concept study**

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3 1 **Automated sequential injection-capillary electrophoresis for dried blood spot analysis: A**  
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5 2 **proof-of-concept study**  
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35 15 **Keywords**  
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37 16 Automation; Dried blood spots; Sequential injection analysis; Capillary electrophoresis;  
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39 17 Capacitively coupled contactless conductivity detection; Clinical analysis  
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3 18 **ABSTRACT:** A hyphenated analytical platform that enables fully automated analyses of dried  
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5 19 blood spots (DBSs) is proposed by the at-line coupling of sequential injection (SI) to capillary  
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7 20 electrophoresis (CE). The SI system, exploited herein for the first time for unattended DBS  
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9 21 handling, serves as the ‘front end’ mesofluidic platform for facilitating exhaustive elution of  
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11 22 the entire DBS by flow programming. The DBS eluates are thus free from hematocrit and non-  
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13 23 homogeneity biases. The SI pump transfers the resulting DBS eluates into CE sample vials  
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15 24 through an internal port of the CE instrument and homogenizes the eluates, whereupon the  
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17 25 eluted blood compounds are automatically injected, separated, and quantified by the CE  
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19 26 instrument. The SI and CE are commercially available off-the-shelf instruments, and are  
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21 27 interconnected through standard nuts, ferrules, and tubing without additional instrumental  
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23 28 adjustments. They are controlled by dedicated software and are synchronized for a fully  
24  
25 29 autonomous operation. The direct determination of endogenous (potassium and sodium) and  
26  
27 30 exogenous (lithium as a model drug) inorganic cations in DBS samples has been used for the  
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29 31 proof-of-concept demonstration. The hyphenated SI-CE platform provides excellent precision  
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31 32 of the analytical method with RSD values of peak areas below 1.5% and 3.5% for intra-day and  
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33 33 inter-day analyses, respectively, of the endogenous concentrations of the two inorganic cations.  
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35 34 For the determination of lithium, calibration is linear in a typical clinical range of the drug ( $R^2$   
36  
37 35 better than 0.9993 for 2 – 20 mg/L), RSD values of peak areas are below 4.5% (in the entire  
38  
39 36 calibration range), limit of detection (0.4 mg/L) and limit of quantification (1.3 mg/L) are well  
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41 37 below the drug’s minimum therapeutic concentration (4 mg/L), and total analysis time is shorter  
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43 38 than 5 min. The SI-CE platform reflects the actual trends in the automation of analytical  
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45 39 methods, offers rapid and highly flexible DBS elution/analysis processes, and might thus  
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47 40 provide a general solution to modern clinical analysis as it can be applied to a broad range of  
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49 41 analytes and dried biological materials.  
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## 42 INTRODUCTION

43 Micro-sampling of dried blood spots (DBSs) has been suggested as a viable alternative to  
44 venous blood collection and has been accepted for specific clinical assays.<sup>1</sup> Standard DBS  
45 sampling involves the collection of a microliter volume of capillary blood onto a paper-based  
46 sampling card from a finger or a heel prick. The collected blood is then dried up in ambient air  
47 for several hours to form the DBS.<sup>2</sup> Since the collected biological material is dry, DBSs are  
48 considered non-biohazardous, can be transported by mail, and can be stored at very simple and  
49 inexpensive conditions. Analytes in DBSs exhibit better stability in comparison to wet blood  
50 samples because enzymes and other reactive compounds are deactivated during the drying  
51 process.<sup>2</sup> Moreover, the collection of capillary blood is more acceptable for most clinical  
52 subjects (specifically for individuals with severe anemia, infants, and children), and DBS  
53 sampling might thus open new horizons in clinical analysis<sup>3-4</sup> and personalized healthcare.<sup>5</sup>  
54 Besides the formerly-evidenced advantages, collection and analysis of DBS face some  
55 challenges, too. DBSs are typically pretreated by multiple-step processes, which are tedious,  
56 time-consuming, and costly. They include sub-punching of a small part of the DBS, which is  
57 then eluted by vigorous shaking, and the resulting eluate is extracted, centrifuged, evaporated,  
58 and reconstituted with a solvent compatible with the subsequent analytical technique.<sup>2</sup> In  
59 addition, DBS analyses are associated with sensitivity issues due to the minute initial blood  
60 volumes and with compromised reliability of quantitative data due to the hematocrit effects and  
61 non-homogenous analyte distribution.<sup>6-7</sup> Recently, novel concepts based upon blood volume-  
62 related corrections,<sup>8</sup> volumetric absorptive microsampling (VAMS),<sup>9</sup> and end-to-end  
63 capillaries<sup>10-11</sup> were proposed to avoid the detrimental effects of DBS collection on quantitative  
64 DBS analyses and to simplify DBS collection. Even though these alternatives have improved  
65 and simplified DBS collection, the subsequent DBS treatment has remained the major challenge  
66 in contemporary DBS analysis because it is performed manually in most assays.<sup>2</sup>

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3 67 To avoid the manual DBS treatment, semi(automated) robotic stations for the hyphenation of  
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5 68 the DBS to liquid chromatography (HPLC)<sup>2, 12</sup> and for the direct injection from DBS into mass  
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7 69 spectrometry (MS)<sup>2, 13</sup> have been presented. However, the automation of the DBS  
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10 70 processing/analysis is not mature yet and there is still a quest of easier, cheaper, and fully  
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12 71 unmanned systems. The major deficiencies of the current (semi)automated systems identified  
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14 72 so far are: (i) the transfer of the DBS cards to the robotic systems by laboratory staff, (ii) the  
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16 73 elution of a sub-section of the original DBS, (iii) the low elution efficiency, (iv) the coelution  
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18 74 of matrix components into the separation/detection system, (v) the high complexity and rigidity  
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20 75 of the processes, and (vi) the high cost of the robotic analytical systems.<sup>2</sup> As a consequence of  
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22 76 (i), manual handling of biological material is necessary, of (ii), quantitative analyses are  
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24 77 hematocrit-dependent, of (ii and iii), costly analytical systems with high sensitivity are  
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26 78 employed, of (iv), separation/spectral interferences and ion suppression are encountered, and  
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28 79 of (v and vi), two stand-alone instruments (for the DBS elution and the eluate analysis) are  
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30 80 required, which make the system highly complex and not affordable for most laboratories.  
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35 81 Flow injection (FI) and related mesofluidic systems were originally conceived to simplify the  
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37 82 analytical workflows and to lower the burden of routine laboratories while outperforming  
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39 83 robotic stations in terms of affordability and versatility.<sup>14-15</sup> Flow-through approaches are based  
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41 84 on monitoring reactions under non-steady-state conditions for high-throughput assays, yet  
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43 85 assuring repeatable timing of events with minimal operator intervention.<sup>16</sup> The second  
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45 86 generation of FI, so-called sequential injection (SI), capitalizes on programmable flow under  
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47 87 user-friendly software control, i.e., a single system can be programmed for a plethora of unit  
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49 88 operations and reaction schemes without the need for system reconfiguration, by exploiting a  
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51 89 bidirectional pump and a multi-position selection valve.<sup>17</sup> As a result, SI-based fluidic systems  
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53 90 are regarded as the most appropriate vehicles for automation of sample preparation, including  
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55 91 liquid-phase (micro)extraction, sorptive (micro)extraction, and leaching procedures.<sup>18-19</sup>  
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3 92 Indeed, the handling and leaching/extraction of solid and dried samples (usually foodstuff or  
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5 93 environmental matrices) is greatly simplified and accelerated by resorting to FI/SI approaches<sup>20-</sup>  
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7 94 <sup>21</sup> that are readily tailor-made to the user's demands. Yet, to our best knowledge, the  
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10 95 exploitation of FI/SI as a front end to modern analytical instrumentation for autonomous  
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12 96 processing of DBSs has not been reported to date.

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14 97 Capillary electrophoresis (CE) offers a cheap, simple, and highly efficient instrumental  
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16 98 configuration, which is perfectly suited to simplify sample processing and analyze minute  
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18 99 volumes of biological samples.<sup>22-24</sup> Besides, commercial CE systems are equipped with an  
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20 100 internal port, which can straightforwardly connect the CE autosampler with an external liquid  
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22 101 handling device.<sup>25</sup> Thus, samples processed with, e.g., an SI system, can be directly transferred  
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24 102 into sample vials in the CE autosampler for at-line CE analyses. The reagents/sample volumes  
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26 103 handled by SI and those typically used in CE are perfectly compatible and this is one of the key  
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28 104 aspects for the ease of coupling of these two techniques. Another pivotal issue of such coupling  
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30 105 is the use of CE as the analytical end for (i) rapid separations with high separation efficiencies,  
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32 106 (ii) high tolerance to common interferences encountered in biological samples, and (iii)  
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34 107 potential on-capillary concentration.<sup>26-28</sup> CE has been recently also shown suitable for an all-  
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36 108 in-one concept enabling processing and analyses of DBSs using a single off-the-shelf  
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38 109 instrument.<sup>11</sup> Despite this achievement, it is still rather difficult to perform fully automated,  
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40 110 flexible, and comprehensive DBS pretreatment by a single CE instrument. We believe that the  
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42 111 high flexibility of the DBS treatment can be obtained by the direct coupling of an autonomous  
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44 112 liquid handling device, such as SI, to CE. The first SI-CE couplings were reported at the turn  
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46 113 of the millennium.<sup>29-30</sup> Nevertheless, the SI systems were merely employed for liquid sample  
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48 114 delivery to the separation capillary end for split-mode injections. It should be also noted that  
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50 115 the hyphenation has been realized preferably with lab-made CE instruments, has mostly been  
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52 116 applied to "clean" samples and has not been used for handling solid/dry samples.<sup>31-32</sup> In fact,  
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3 117 coupling of flow-through DBS processing by mesofluidic platforms to CE analysis has not been  
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5 118 described as of yet.

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7 119 In order to resort to the favorable synergetic aspects of SI and CE and to complement/broaden  
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9 the portfolio of automated DBS analytical set-ups, the actual contribution presents the proof-  
10 120 of-concept of a novel, fully automated SI-CE platform for DBS analysis. To this end, we aim  
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12 121 at the autonomous elution of the entire DBS (thus free from hematocrit and non-homogeneity  
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14 122 effects) with an SI system that will be at-line coupled to the internal autosampler of a CE  
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16 123 instrument. Investigation of critical parameters for flow-through DBS elution will be  
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18 124 investigated in details. Performance characteristics of the automated SI-CE system for DBS  
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20 125 analysis will be compared with the standard DBS elution methodology by the determination of  
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22 126 endogenous and exogenous ionic species in DBSs at physiologically relevant concentrations.  
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3 128 **EXPERIMENTAL SECTION**  
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5 129 **Reagents, Standard Solutions, and DBS Samples.** Details on reagents and standard solutions  
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8 130 are described in *Supporting Information*. DBS samples were formed by spotting 10  $\mu\text{L}$  of  
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10 131 capillary blood from a finger prick onto Whatman<sup>TM</sup> 903 Protein Saver sampling card (GE  
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12 132 Healthcare Ltd, Cardiff, UK) and by drying the spots at laboratory temperature for 3 h. The  
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14 133 DBS samples were analyzed the day after collection. Written informed consent was signed by  
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17 134 all donors of the DBS samples. Other details on DBS sampling can be found in an earlier  
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19 135 contribution.<sup>8</sup>  
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23 137 **Capillary Electrophoresis Apparatus.** CE analyses were performed with a 7100 CE  
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25 138 instrument (Agilent Technologies, Waldbronn, Germany) equipped with an Admet capacitively  
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27 139 coupled contactless conductivity detector (C<sup>4</sup>D) (Admet, Prague, Czech Republic). Other  
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29 140 details can be found in *Supporting Information*.  
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35 142 **Sequential Injection System.** The components of the SI system are schematically illustrated  
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37 143 in the right panel of **Figure 1**. The mesofluidic MicroSIA system was purchased from FIALab  
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39 144 Instruments Inc. (Seattle, WA, USA) and employed a low-pressure metal-free 8-position  
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41 145 selection valve and a 30 mm-stroke bi-directional syringe pump. A 3-way head valve allowed  
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43 146 the connection of the syringe pump to the carrier solution (deionized (DI) water), air, and the  
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45 147 flow pathway via a 65 cm-long holding coil (HC1, 1.0 mm i.d./1.6 mm o.d. perfluoroalkoxy  
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47 148 (PFA) tubing, Vici-Jour, Schenkon, Switzerland). A 500  $\mu\text{L}$ -borosilicate glass syringe (XC/XP  
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49 149 with PTFE plunger tip seal, Tecan Systems, Inc., San Jose, CA, USA, P/N 20725590) was used  
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51 150 for automatic liquid handling. The peripheral ports #2 and #3 of the selection valve served for  
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53 151 the autonomous aspiration of air and elution solution through the communication channel into  
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55 152 HC1, and port #1 was used for liquid disposal to waste. Tubing connected to ports #1, #2, and  
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3 153 #3 were 10 cm-long segments of PFA tubing (1.0 mm i.d./1.6 mm o.d., Vici-Jour). Unattended  
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5 154 control of all flow system units (syringe pump, head valve, selection valve) was accomplished  
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8 155 via USB using the open-source software CocoSoft (version 5.15) written in Python  
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10 156 programming language.<sup>33</sup> An initial SI system flushing sequence was carried out at the  
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12 157 beginning of each working day and is presented in **Table S1** in *Supporting Information*.

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17 159 **DBS Elution Device.** The DBS elution device (disassembled and assembled) is depicted in  
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19 160 **Figure 2** and is based on a commercial dialysis unit (Harvard Apparatus, Holliston, MA, USA,  
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21 161 P/N 74-0400). The connection between the MicroSIA and the DBS elution device was  
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23 162 accomplished through a 10 cm-long holding coil (HC2, 0.5 mm i.d./1.6 mm o.d. PFA tubing,  
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25 163 Vici-Jour) connected to port #4 of the selection valve. A leak-free connection at the DBS elution  
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27 164 device inlet was achieved by pushing the end of the HC2 into a 1 cm-long segment of silicone  
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29 165 tubing (1 mm i.d./3 mm o.d., Gumex, Strážnice, Czech Republic). A DBS disc (11 mm) was  
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31 166 placed into the DBS holder together with a silicone O-ring (8 mm i.d./11 mm o.d., 1 mm thick,  
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33 167 Zlíntech, Zlín, Czech Republic) and the two parts of the device (holder + nut) were screwed  
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35 168 together. The connection between the outlet of the device and the CE replenishment needle  
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37 169 assembly was realized by a 15 cm-long holding coil (HC3, 0.5 mm i.d./1.6 mm o.d. PFA tubing,  
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39 170 Vici-Jour), which acted as the transfer line from SI to CE. A leak-free connection at the DBS  
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41 171 elution device outlet was achieved by pushing the end of the HC3 into a 1 cm-long segment of  
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43 172 silicone tubing (1 mm i.d./3 mm o.d., Gumex).

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47 174 **Off-line DBS Elution Procedures. SI Elution.** Preliminary tests involving off-line SI elution  
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49 175 of DBS samples were performed according to the following procedure. (i) The entire DBS was  
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51 176 punched from the sampling card using an 11 mm cork-borer. (ii) The resulting disc with the  
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53 177 DBS and a silicone O-ring were placed into the DBS holder and the holder and the nut were  
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3 178 screwed together. (iii) The DBS was eluted with DI water using the MicroSIA and the resulting  
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5 179 eluate was collected into a 250  $\mu\text{L}$  plastic vial. The eluate was homogenized by agitation at  
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7 180 1000 rpm for 60 s and 50  $\mu\text{L}$  was transferred to a CE micro-vial (Agilent Technologies, P/N  
8  
9 181 9301-0978) for injection.

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12 182 **DBS Agitation.** Details on the standard protocol for DBS elution by agitation can be found in  
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14 183 *Supporting Information.*

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19 185 **At-line SI-CE Coupling.** Schema and components of the platform for the autonomous SI-CE  
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21 186 analyses of DBSs are graphically presented in **Figure 1**. The DBS elution device was assembled  
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23 187 identically to the procedure reported in section *DBS Elution Device*. The operation of the SI  
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25 188 system was identical to that described in section *Off-line DBS Elution Procedures. SI Elution*  
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27 189 with the exception that the DBS eluate was autonomously transferred to an empty glass snap-  
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29 190 cap vial in the replenishment lift of the CE instrument through the transfer line (HC3). The  
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31 191 eluate was then autonomously homogenized by a stream of air delivered by the MicroSIA pump  
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33 192 directly to the CE vial and the replenishment lift moved the vial to the autosampler carousel for  
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35 193 subsequent CE injection/analysis. The connection between the SI and the CE system is  
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37 194 graphically presented in **Figure S1** in *Supporting Information*. The original tubing connecting  
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39 195 the CE replenishment needle with the CE replenishment system was disconnected from port A  
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41 196 of the replenishment needle assembly. Subsequently, the outlet of HC3 was screwed into port  
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43 197 A. Connection to port B (liquid level sensor) of the replenishment needle assembly was not  
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45 198 modified.  
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3 199 **RESULTS AND DISCUSSION**  
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5 200 **Manual DBS Elution.** Manual DBS elution<sup>8</sup> was used as a reference procedure for the  
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7 201 comparison with the newly developed DBS elution procedure using the SI system and is  
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9 202 detailed in **Figure S2** and the corresponding text in *Supporting Information*. Maximum DBS  
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11 203 elution efficiency was achieved in 15 min and was used for all manual DBS elutions.  
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13 204 Interestingly, the calculated elution efficiency showed an unexpected positive bias for Na<sup>+</sup>  
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15 205 eluted from DBSs with maximum efficiencies  $\geq 100\%$ . This discrepancy has been investigated  
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17 206 in detail in *SI Elution of Inorganic Cations from DBS* and has been identified as a cross-  
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19 207 contamination resulting from the DBS sampling material.  
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26 209 **Configuration of the Flow-Through SI system.** The settings and connections of the SI system  
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28 210 and the related flow pathways were comprehensively examined for reliable flow-through  
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30 211 elution of DBS. This included investigation of the connections between the head valve and the  
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32 212 selection valve of the SI system, and between the selection valve of the SI system and the DBS  
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34 213 elution device. Moreover, the DBS disc size and the internal chamber layout of the DBS elution  
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36 214 device were explored as well as the parameters of the outlet tubing from the DBS elution device,  
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38 215 i.e. the transfer line to CE. The selected dimensions and lengths were 1.0 mm i.d. and 65 cm  
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40 216 for the tubing interconnecting the head valve and the selection valve of the SI system (HC1),  
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42 217 0.5 mm i.d. and 10 cm for the tubing interconnecting the selection valve and the DBS elution  
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44 218 device (HC2), and 0.5 mm i.d. and 15 cm for the outlet tubing from the DBS elution device  
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46 219 (HC3, transfer line). The dimensions/lengths were chosen to ensure sufficient volume of HC1  
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48 220 ( $\sim 510 \mu\text{L}$ ) for a full-stroke operation of the  $500 \mu\text{L}$  syringe pump, and the minimum feasible  
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50 221 volume of HC2 and HC3 for the transfer of the eluent to and the eluate from the DBS elution  
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52 222 device, respectively. More details can be found in *Supporting Information*.  
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3 223 The DBS holder used in this work has an internal chamber that accommodates DBS discs with  
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5 224 a diameter up to 11.6 mm. The 10  $\mu\text{L}$  volume of capillary blood forms a DBS with a 6-7 mm  
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8 225 diameter. A DBS disc size of 11 mm that ensures a whole DBS punch and a constant position  
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10 226 of the disc inside the holder was, therefore, selected. Initial experiments with the holder, the  
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12 227 DBS disc, and the nut screwed together revealed (leak-free) elution of the central part of the  
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14 228 DBS only (see **Figure S3** in *Supporting Information*). This was caused by the fact that the  
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17 229 eluent stream did not efficiently wet and elute the peripheral parts of the DBS disc covered by  
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19 230 the nut. As we have aimed at the DBS elution free from hematocrit/non-homogeneity effects,  
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21 231 the layout of the DBS holder was slightly modified to achieve exhaustive DBS elution. A 1 mm  
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24 232 thick silicone O-ring (8 mm i.d./11 mm o.d.) was placed onto the DBS disc before the DBS  
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26 233 elution device was screwed together. This formed an internal cavity above the DBS (with a  
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28 234 constant volume and a diameter larger than the DBS), which ensured the intimate contact of the  
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30 235 eluent with the DBS card and thus fostered the elution of the entire DBS.

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35 237 **SI Hydrodynamic Characteristics for Off-line DBS Elution.** The hydrodynamic parameters  
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37 238 of the SI setup for the DBS elution were initially examined with an eluate volume of 250  $\mu\text{L}$ .  
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39 239 For the DBSs formed by spotting 10  $\mu\text{L}$  of capillary blood, the dilution factor was 25 and was  
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41 240 selected based on our previous experience; the 25-diluted DBS eluates ensured repeatable and  
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43 241 interference-free CE analyses of target analytes with minimum capillary maintenance.<sup>8</sup> The  
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45 242 ruggedness of the SI system for DBS processing under flow-through conditions was examined  
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47 243 using different configurations and flow rates, and the resulting performance is summarized in  
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50 244 **Table 1**. First, the DBS elution device was used without the DBS disc and 250  $\mu\text{L}$  of DI water  
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52 245 was flushed through the SI pathway followed by 250  $\mu\text{L}$  of air. A flow rate of 300  $\mu\text{L}/\text{min}$  was  
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54 246 selected as a suitable liquid transfer speed that offers a reasonably short elution time but a  
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56 247 sufficiently long contact time based on the results presented in *SI elution of inorganic cations*  
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3 248 *from DBS*. The transferred liquid was collected at the outlet of HC3, weighted, and the liquid  
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5 249 volume was calculated according to equation (1) in *Supporting Information*. Second, a DBS  
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7 250 disc with no capillary blood was placed in the DBS elution device, the SI flushed 250  $\mu\text{L}$  of DI  
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9 251 water and 250  $\mu\text{L}$  of air consecutively through the device at 300  $\mu\text{L}/\text{min}$ , and the transferred  
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11 252 liquid was collected and its volume calculated as previously. Finally, a DBS disc with 10  $\mu\text{L}$  of  
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13 253 blood was placed in the DBS elution device, consecutively flushed with 250  $\mu\text{L}$  of DI water  
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15 254 and 250  $\mu\text{L}$  of air, and the transferred liquid was collected and its volume calculated as  
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17 255 previously. DBSs were eluted at five different flow rates ranging from 150 to 2000  $\mu\text{L}/\text{min}$  (see  
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19 256 **Table 1**). For a comparison, DBSs were also eluted by the standard protocol according to  
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21 257 *Manual DBS elution* (see above), the eluate was recovered by pipetting out all free liquid from  
22  
23 258 the vial and its volume was calculated as previously.

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26 259 The results demonstrate an accurate liquid transfer by SI (246.8  $\mu\text{L}$ ) through the empty DBS  
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28 260 holder with excellent repeatability (0.3% RSD). The slightly lower absolute volume can be  
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30 261 ascribed to the precision of glass syringe manufacturing, which is usually around 1%. The eluate  
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32 262 volumes collected after elution of blank and blood-spotted DBS discs were 20.8 and 24.0  $\mu\text{L}$   
33  
34 263 less, thus indicating some adsorption of the eluent solution by the cellulose-based DBS  
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36 264 sampling material. Similarly, DBSs eluted at different flow rates indicate similar adsorption of  
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38 265 the eluent (20.2 – 22.6  $\mu\text{L}$ ) by the DBS discs regardless of the eluent flow rate. The repeatability  
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40 266 of the elution process was slightly worsened whenever DBS discs were processed and this might  
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42 267 be attributed to the manual sub-punching of the discs and the slight differences in homogeneity  
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44 268 of the sampling material. Nevertheless, RSD values were in all instances better than 1.9%,  
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46 269 thereby again demonstrating excellent repeatability of the SI-driven DBS elution process. In  
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48 270 addition, the volume collected after the DBS elution with the SI system is in all instances higher  
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50 271 and more repeatable than that after the manual DBS elution. These results also suggested that  
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3 272 the SI-based automated elution is more amenable to DBS processing with lower elution  
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5 273 volumes for improved sensitivity (see **Figure 4** later in the manuscript).  
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10 275 **SI Elution of Inorganic Cations from DBS.** To further evaluate the efficiency of the SI system  
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12 276 for flow-through DBS elution at different flow rates, the collected eluates were analyzed by  
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14 277 CE-C<sup>4</sup>D for the quantitative determination of endogenous inorganic cations. Capillary blood  
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16 278 contains ~ 100 mM concentrations of K<sup>+</sup> and Na<sup>+</sup> and 2 – 3 orders of magnitude lower  
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18 279 concentrations of Ca<sup>2+</sup>, Mg<sup>2+</sup>, and NH<sub>4</sub><sup>+</sup>.<sup>8</sup> The two major cations were considered in our  
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20 280 experiments and their concentrations in DBS eluates after SI treatment were compared with  
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22 281 their concentrations in DBS eluates prepared according to *Manual DBS elution* reported earlier.  
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24 282 The elution efficiency values achieved at 150, 300, 600, 1200, and 2000  $\mu\text{L}/\text{min}$  flow rates are  
25  
26 283 depicted in **Figure 3** along with the duration of the total elution procedure. The increase of the  
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28 284 flow rate from 150 to 2000  $\mu\text{L}/\text{min}$  decreased the elution time by a factor of 5.6. The total  
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30 285 elution procedure at 2000  $\mu\text{L}/\text{min}$  took 40 s, which is 22.5-fold faster than the manual DBS  
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32 286 elution. On the other hand, elution efficiency at 2000  $\mu\text{L}/\text{min}$  was slightly compromised (~  
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34 287 80%) because the contact time of the elution solution with the DBS had been reduced to 7.5 s  
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36 288 only. The incomplete DBS elution was clearly observed by visual inspection of the DBS discs  
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38 289 and is demonstrated in **Figure S4** in *Supporting Information*. Elution efficiencies were rather  
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40 290 consistent (94 – 98%, RSD  $\leq$  3.1%) for 150 – 600  $\mu\text{L}/\text{min}$  flow rates, and 600  $\mu\text{L}/\text{min}$  was  
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42 291 selected for subsequent experiments (with 250  $\mu\text{L}$  elution volume) due to the faster elution  
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44 292 procedure (merely 75 s).  
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51 293 The elution volume determines the actual blood dilution factor of the final DBS eluate. In fact,  
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53 294 various dilution factors might be required based on the analyte's blood concentration and the  
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55 295 complexity of the resulting eluate. The flexibility of the SI system for the DBS elution was  
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57 296 demonstrated by the autonomous handling of various elution volumes (75 – 250  $\mu\text{L}$ ), which  
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3 297 resulted in blood dilution factors within the range of 7.5 – 25. The elution flow rate was here  
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5 298 decreased down to 300  $\mu\text{L}/\text{min}$  to ensure a reasonable contact time with the DBS for the  
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7 299 smallest eluent volumes and was later further investigated in a separate procedure. The results  
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10 300 in **Figure 4** demonstrate a linear increase of collected eluate volumes in the 75 – 250  $\mu\text{L}$  range.  
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12 301 The collected eluate volumes were lower by approximately 25  $\mu\text{L}$  in comparison to the original  
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14 302 elution volumes, and the volume reduction was consistent with the volumes adsorbed by the  
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16 303 DBS sampling discs reported in **Table 1**. Concentrations of the inorganic cations in the DBS  
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18 304 eluates increased for reduced elution volumes and peak areas for  $\text{K}^+$  and  $\text{Na}^+$  were 2.9 and 2.8-  
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20 305 fold higher for 75 vs. 250  $\mu\text{L}$  eluate volumes, respectively. These values were slightly lower  
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22 306 than the theoretically calculated increase (3.33-fold) and were caused by the non-exhaustive  
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24 307 elution of DBS compounds at the herein selected SI conditions (elution volume and flow rate).  
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26 308 The repeatability of the DBS elution protocol for the 75  $\mu\text{L}$  elution volume (RSD 10.1 – 11.6%)  
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28 309 worsened considerably compared to 250  $\mu\text{L}$  (RSD 1.3 – 1.4%) and was also ascribed to the  
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30 310 incomplete elution of the DBS compounds at the selected SI conditions. The SI system was  
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32 311 capable of handling even lower volumes of the DBS elution solution and the minimum volume  
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34 312 was approx. 35  $\mu\text{L}$  due to the liquid absorption by the DBS disc (approx. 25  $\mu\text{L}$ ). Nevertheless,  
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36 313 application of such low volumes resulted in an even more compromised elution repeatability,  
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38 314 minute volumes and increased matrix complexity of collected eluates, excessive saponification  
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40 315 during at-line eluate homogenization, and required additional adjustments of the SI-CE set-up.  
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42 316 A comprehensive investigation of all these aspects was beyond the scope of the actual proof-  
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44 317 of-concept study and DBS elution with minute eluate volumes will be elaborated in detail in a  
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46 318 subsequent study.  
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48 319 The effect of the SI operational conditions on the DBS elution was further examined for just a  
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50 320 10-fold dilution factor using an elution volume of 100  $\mu\text{L}$  and elution flow rates of 150 – 1200  
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52 321  $\mu\text{L}/\text{min}$ . The dilution factor can be automatically adjusted by programming adequate elution  
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3 322 volume in the SI script. The resulting elution times and elution efficiency values for  $K^+$  and  $Na^+$   
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5 323 are depicted in **Figure 5**. Higher flow rates demonstrate faster elution procedures (0.8 min for  
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7 324  $1200 \mu\text{L}/\text{min}$  vs. 1.4 min for  $150 \mu\text{L}/\text{min}$ ), however, at the expense of reduced elution efficiency  
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9 325 and repeatability. The elution efficiency values dropped down to 80% (RSD  $\sim 4.1\%$ ) and 60%  
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11 326 (RSD  $\sim 8.1\%$ ) for  $600 \mu\text{L}/\text{min}$  and  $1200 \mu\text{L}/\text{min}$ , respectively. Elution of DBSs at low dilution  
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13 327 factors is therefore recommended at low flow rates ( $\leq 300 \mu\text{L}/\text{min}$ ) so as to enable nearly  
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15 328 exhaustive elution of  $K^+$  and  $Na^+$  from the DBS (93 – 95%) with excellent repeatability (RSD  
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17 329  $\leq 2.4\%$ ) and elution times  $\leq 85$  s.

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21 330 An interesting artifact was observed in the CE- $C^4D$  electropherograms resulting from the two  
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23 331 elution procedures (manual vs. automated DBS elution). Analytical signals for the low abundant  
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25 332 inorganic cations ( $NH_4^+$  and  $Ca^{2+}$ ) were considerably higher for the eluates prepared by the  
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27 333 manual DBS elution. To prove our hypothesis that their increased concentrations are caused by  
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29 334 the DBS sampling material and/or by the DBS processing procedure, five different samples  
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31 335 were prepared and analyzed. CE- $C^4D$  electropherograms of the five samples are depicted in  
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33 336 **Figure S5** in *Supporting Information*. In brief, a standard blood sample was prepared by  
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35 337 diluting  $10 \mu\text{L}$  of liquid capillary blood with  $240 \mu\text{L}$  of DI water. One blank eluate was prepared  
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37 338 by the automated and another one by the manual elution of blood-free sampling discs. One DBS  
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39 339 eluate was prepared by the automated and another one by the manual elution of sampling discs  
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41 340 with  $10 \mu\text{L}$  DBSs. In comparison to the standard blood sample, increased peak areas were  
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43 341 observed for  $NH_4^+$ ,  $Ca^{2+}$ , and  $Na^+$  in the manually prepared DBS eluate. Manual elution of a  
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45 342 blood-free DBS disc revealed a considerable release of  $NH_4^+$ ,  $Ca^{2+}$ , and  $Na^+$  into the eluate,  
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47 343 which rationalized the observed increase of their CE peak areas in the DBS eluate. Under the  
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49 344 DBS elution conditions employed, the peak areas increased by 107%, 1%, 226%, and 11% for  
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51 345  $NH_4^+$ ,  $K^+$ ,  $Ca^{2+}$ , and  $Na^+$ , respectively, and had a significant effect on the quantitative DBS  
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53 346 analysis. On the other hand, the automated SI system resulted in a considerably milder elution  
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3 347 process. In comparison to the manually eluted blood-free DBS disc, the released amounts of  
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5 348  $\text{NH}_4^+$ ,  $\text{K}^+$ ,  $\text{Ca}^{2+}$ , and  $\text{Na}^+$  were 4, 3, 8, and 4-fold lower, respectively. Leaching of the DBS  
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7 349 sampling material components into the eluates has not been reported earlier and might not be  
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9 350 critical for clinical analyses of drugs and other exogenous compounds because they will very  
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11 351 likely not be present in sampling materials. However, it can be detrimental for inorganic  
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13 352 analysis as many inorganic ions are present at trace concentrations in blood and their  
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15 353 determination can be impaired by the DBS material leaching. DBS elution by SI might thus be  
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17 354 advantageous due to the milder and easily controllable elution process. Furthermore, sampling  
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19 355 on alternative materials (such as VAMS<sup>9</sup> or soluble foams<sup>34</sup>), which might be characterized by  
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21 356 reduced leaching of intrinsic inorganic cations, could be beneficial.  
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28 358 **DBS Elution Device Orientation.** Three different orientations of the DBS holder were tested  
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30 359 and the corresponding results are depicted in **Figure S6** and **Table S3** in *Supporting*  
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32 *Information*.  
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37 362 **At-line SI-CE Coupling for a Fully Autonomous DBS Analysis.** After the initial examination  
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39 363 of the SI characteristics for the off-line DBS elution, the SI system and the DBS elution device  
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41 364 were coupled to the inlet port of the replenishment needle assembly (port A, see *Experimental*  
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43 365 *Section*, **Figure 1**, and **Figure S1**) of the commercial CE. The coupling required only standard  
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45 366 nuts, ferrules, and tubing. No adjustment other than unscrewing the original tubing from port A  
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47 367 of the replenishment needle assembly was required. Length (15 cm) and i.d. (0.5 mm) of the  
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49 368 transfer line were carefully selected to ensure minimum dead volume and backpressure.  
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53 369 Both autonomous units (the SI and the CE instrument) were controlled by a single personal  
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55 370 computer, which enabled a full synchronization of SI elution and CE analysis steps. Facile  
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57 371 adjustments of the operational parameters of the SI system during method developments were  
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3 372 performed by CocoSoft freeware. Examples of selected scripts for the initial SI cleaning and  
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5 373 the SI-controlled DBS elution are shown in *Supporting Information*. Full control of the CE  
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7 374 instrument was achieved by ChemStation software, which enabled autonomous manipulation  
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10 375 of CE vials within the autosampler carousel and the replenishment lift. The entire analytical  
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12 376 process ran fully unattended and the description of all program steps and details of the SI-CE  
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14 377 synchronization are shown in **Table S4** and **Table S5** in *Supporting Information*. To examine  
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16 378 the suitability of the at-line SI-CE coupling for the automated flow-through DBS elution, 5  
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18 379 unique DBSs were eluted with 250  $\mu\text{L}$  of DI water at 600  $\mu\text{L}/\text{min}$ . The eluates transferred to  
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21 380 CE sample vials were weighted and recalculated to volume. The average collected eluate  
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23 381 volume was 222.4  $\mu\text{L}$  (2.7% RSD) and was consistent with the volume (and repeatability) of  
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25 382 the off-line DBS eluate collection.

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28 383 The major advantage of the proposed at-line coupling is the synchronization of the overall DBS  
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30 384 analysis steps. DBS elution, eluate transfer to the sample vial, and eluate homogenization (see  
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32 385 next section) were carried out by the SI system and were controlled by CocoSoft.  
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34 386 Simultaneously with the DBS elution, ChemStation performed preconditioning of the  
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36 387 separation capillary (flushing with NaOH and BGE solutions) for the CE analysis. Once the  
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38 388 eluate was ready for analysis and the CE capillary preconditioned, the sample vial was moved  
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41 389 to the CE carousel for injection and the quantitative analysis was immediately initiated. A  
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43 390 considerable reduction of analysis time was thus achieved because the DBS  
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45 391 elution/homogenization and capillary preconditioning were performed simultaneously.  
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47 392 Duration of all respective steps of a typical SI-CE procedure is specified in **Table S4** (75 s for  
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49 393 DBS elution/homogenization, 120 s for capillary preconditioning, 120 s for CE analysis) and  
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51 394 the total DBS analysis time was 280 s per sample (**Table S5** in *Supporting Information*). A 20  
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53 395 s flush with 100 mM NaOH was sufficient for the removal of blood matrix components from  
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55 396 the capillary inner walls (e.g., proteins, after the previous DBS analysis) and ensured excellent  
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3 397 repeatability of migration times of  $K^+$  and  $Na^+$  at their endogenous concentrations. RSD values  
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5 398 for intra-day (5 DBSs in one day,  $n = 5$ ) and inter-day (5 DBSs in one month,  $n = 5$ )  
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7 399 measurements were  $\leq 0.3\%$  and  $1.1\%$ , respectively.  
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12 401 **Autonomous Homogenization of the Collected DBS Eluate.** The DBS eluate collected in a  
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14 402 CE sample vial after the SI elution is rather non-homogenous. This is caused by the gradual  
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16 403 dissolution of the dried blood during the DBS elution procedure that generates a saturated and  
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18 404 diluted DBS eluate at the beginning and at the end of the procedure, respectively (see **Figure**  
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20 405 **S7** in *Supporting Information*). Quantitative analyses might thus be significantly biased if CE  
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22 406 injections are performed from the non-homogenous eluates. The at-line SI-CE coupling offers  
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24 407 a flexible tool for an attractive, quick, and efficient eluate homogenization by SI pumping of a  
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26 408 given volume of air at a given flow rate through the entire SI-CE system until the CE  
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28 409 replenishment needle. The two parameters were investigated in separate procedures detailed in  
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30 410 **Table 2** and in *Supporting Information*. Experimental results revealed that the eluate was well  
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32 411 homogenized, as compared to vortex mixing, by flushing  $250 \mu\text{L}$  of air at  $600 \mu\text{L}/\text{min}$  after the  
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34 412 eluate. Quantitative determination of  $K^+$  and  $Na^+$  at their endogenous concentrations in five  
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36 413 distinct DBS eluates demonstrated intra-day repeatability and inter-day reproducibility of peak  
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38 414 areas better than  $1.5\%$  and  $3.5\%$ , respectively.  
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44 415 A comprehensive description of the SI-CE platform operation and operator's steps during the  
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46 416 autonomous DBS elution/analysis are reported in *Supporting Information*.  
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51 418 **Model Clinical Application.** The proposed at-line SI-CE coupling for fully autonomous DBS  
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53 419 analyses has been further evaluated by the determination of lithium as a clinically relevant  
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55 420 analyte. Lithium is determined in human blood as a drug for the treatment of bipolar disorders.  
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57 421 Lithium therapeutic concentrations are in the  $4 - 8 \text{ mg}/\text{L}$  range and the borderline between the  
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3 422 maximum therapeutic concentration, toxicity (8 – 13 mg/L), and poisoning (16 mg/L) is  
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5 423 relatively narrow.<sup>35</sup> DBSs for the determination of lithium were prepared by spotting and drying  
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7 424 out 10  $\mu\text{L}$  of drug-free capillary blood and the same capillary blood spiked with 2, 5, 10, and  
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9 425 20 mg/L of lithium. The SI elution was performed with 250 and 100  $\mu\text{L}$  of DI water and the  
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11 426 resulting eluates were at-line transferred to CE for the autonomous homogenization, injection,  
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13 427 and analysis. The results are summarized in **Table S6** in *Supporting Information* and  
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15 428 demonstrate excellent repeatability (RSD less than 4.5%) and linearity (coefficients of  
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17 429 determination better than 0.9993) of the analytical technique. Further improvement of the  
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19 430 quantitative parameters might be achieved by the application of an internal standard. The limits  
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21 431 of detection and quantification (LOD and LOQ, defined as 3S/N and 10S/N, respectively) were  
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23 432 1.0 and 3.3 mg/L for the 250  $\mu\text{L}$  and 0.4 and 1.3 mg/L for the 100  $\mu\text{L}$  elution volume,  
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25 433 respectively. These results imply 2.5-fold better LOD/LOQ for the latter elution conditions,  
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27 434 which are consistent with the reduced dilution factor. Sufficient sensitivity for the SI-CE-C<sup>4</sup>D  
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29 435 determination of lithium in clinical samples was observed for both elution volumes. Zoomed  
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31 436 sections of the electropherograms for the five DBSs eluted with 100  $\mu\text{L}$  of DI water are depicted  
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33 437 in **Figure 6** and a full-scale electropherogram demonstrating the separation efficiency, baseline  
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35 438 stability and matrix-related peaks is depicted in **Figure S8** in *Supporting Information*.  
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## 440 CONCLUSIONS

441 A novel hyphenated analytical platform capable of autonomous DBS analyses is herein  
442 presented. An SI system is used as the ‘front end’ manifold for handling minute volumes of  
443 solutions and facilitating the fully unattended DBS elution from a customized DBS elution  
444 device. The flow manifold is furnished with a multi-position selection valve and bidirectional  
445 syringe pump for flexible SI-based manipulations of elution solutions. Their volumes and flow  
446 rates might be investigated at will by flow programming to ensure the elution of the entire DBS

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3 447 in the shortest possible time. The outflow of the DBS elution device is connected to an internal  
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5 448 port of a CE instrument for the at-line SI-CE coupling. This coupling enables the automated  
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7 449 transfer of the resulting DBS eluate to a sample vial in the CE autosampler by the SI pump,  
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9 450 followed by the autonomous injection, separation, and quantification of the eluted blood  
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11 451 components by the CE system. The SI and CE are commercially available off-the-shelf  
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13 452 instruments, and are interconnected through standard nuts, ferrules, and tubing. The only  
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15 453 adjustment to the original instruments is the disconnection of the internal tubing from the CE  
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17 454 replenishment assembly device and its replacement with the outflow from the DBS elution  
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19 455 device. The instruments are controlled by dedicated software and are synchronized for a fully  
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21 456 unattended operation. Moreover, the SI-CE coupling offers reliable liquid handling, rapid  
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23 457 analysis, and sufficient sensitivity for the determination of endogenous and exogenous DBS  
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25 458 compounds. The proposed proof-of-concept study reflects the actual trends in automation of  
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27 459 analytical techniques and provides a general solution to modern clinical analysis as it can be  
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29 460 applied to a broad range of analytes and dried biological materials. Moreover, sensitivity and  
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31 461 selectivity of this concept might be further enhanced by the at-line coupling of SI to CE with  
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33 462 ESI-MS detection because it has been proven recently that interferences from blood matrix were  
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35 463 not observed and DBS eluates were fully compatible with CE-ESI-MS in isotachophoretic  
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37 464 mode.<sup>36</sup>  
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5 473 The authors declare no conflict of interest.  
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10 475 **SUPPORTING INFORMATION**  
11

12 476 (i) Experimental Section details, (ii) DBS elution by agitation, (iii) SI-CE connection, (iv) off-  
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14 477 line DBS elution by SI, (v) electropherograms for cross-contamination/interference study, (vi)  
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16 478 CocoSoft scripts, (vii) orientation of the DBS elution device, (viii) homogenization of DBS  
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18 479 eluates, (ix) SI-CE synchronization flow-charts, (x) SI-CE operation.  
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3 576 **Figure Captions**  
4

5 577 Figure 1. Schematic illustration of the at-line SI-CE coupling for the automated DBS elution  
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7 578 and analysis. HC1 – holding coil 1, HC2 - holding coil 2, HC3 – holding coil 3.  
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10 579  
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12 580 Figure 2. Sketch of the components of the DBS elution device (disassembled and assembled).  
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14 581  
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16 582 Figure 3. The effect of the flow rate on the DBS elution efficiency and the total elution time.  
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18 583 DBS parameters and SI conditions as for **Table 1**; CE conditions, see *Experimental Section* in  
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20 584 *Supporting Information*,  $n = 5$ .  
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24 585  
25  
26 586 Figure 4. The effect of the elution volume on the peak areas of inorganic cations eluted from  
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28 587 DBSs and the collected eluate volume. SI conditions: elution flow rate, 300  $\mu\text{L}/\text{min}$ ; elution  
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30 588 solution, DI water; DBS parameters and CE conditions as for **Figure 3**,  $n = 5$ .  
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35 590 Figure 5. The effect of the flow rate on the DBS elution efficiency and the total elution time.  
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37 591 DBS parameters and CE conditions as for **Figure 4**, SI conditions: elution solution, 100  $\mu\text{L}$  of  
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39 592 DI water,  $n = 5$ .  
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42 593  
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44 594 Figure 6. Autonomous SI-CE-C<sup>4</sup>D determination of lithium in DBS samples. DBS parameters  
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46 595 and CE conditions as for **Figure 4**. SI conditions: elution flow rate, 300  $\mu\text{L}/\text{min}$ ; elution  
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48 596 solution, 100  $\mu\text{L}$  of DI water; spiked lithium concentrations: a – 0 mg/L, b – 2 mg/L, c – 5  
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50 597 mg/L, d – 10 mg/L, e – 20 mg/L.  
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598 Table 1. Hydrodynamic parameters of the SI system for the DBS elution as compared with the  
 599 standard agitation procedure. DBS parameters: blood volume, 10  $\mu\text{L}$ ; disc size, 11 mm. SI  
 600 conditions: elution solution, 250  $\mu\text{L}$  of DI water; for full SI program, see **Table S2** in  
 601 *Supporting Information*;  $n = 5$ .

|   |                  |                  |                  |                  |                  |                   |                   |                    |
|---|------------------|------------------|------------------|------------------|------------------|-------------------|-------------------|--------------------|
| Eluent flow rate ( $\mu\text{L}/\text{min}$ ) | 300 <sup>a</sup> | 300 <sup>b</sup> | 150 <sup>c</sup> | 300 <sup>c</sup> | 600 <sup>c</sup> | 1200 <sup>c</sup> | 2000 <sup>c</sup> | n.a. <sup>e</sup>  |
| Total elution time (s)                        | 125              | 125              | 225              | 125              | 75               | 50                | 40                | 900 <sup>e</sup>   |
| Contact time <sup>d</sup> (s)                 | n.a.             | 50               | 100              | 50               | 25               | 12.5              | 7.5               | 900 <sup>e</sup>   |
| Collected eluate volume ( $\mu\text{L}$ )     | 246.8            | 222.8            | 226.6            | 226.0            | 226.2            | 225.6             | 224.2             | 204.2 <sup>e</sup> |
| RSD (%)                                       | 0.3              | 1.1              | 1.8              | 1.2              | 1.9              | 1.4               | 1.6               | 3.7 <sup>e</sup>   |

602  
 603 <sup>a</sup> – SI elution with no DBS disc  
 604 <sup>b</sup> – SI elution of a blank DBS disc with no capillary blood  
 605 <sup>c</sup> – SI elution of a DBS disc with 10  $\mu\text{L}$  of capillary blood  
 606 <sup>d</sup> – Contact time of eluent with the DBS  
 607 <sup>e</sup> – DBS agitation at 1000 rpm for 15 min  
 608 n.a. – not applicable

610 Table 2. SI-driven homogenization of the collected DBS eluates. DBS parameters and CE  
 611 conditions as for **Figure 3**, SI conditions: elution flow rate, 600  $\mu\text{L}/\text{min}$ ; elution solution, 250  
 612  $\mu\text{L}$  of DI water;  $n = 3$ .

| Elution volume ( $\mu\text{L}$ ) | Eluent flow rate ( $\mu\text{L}/\text{min}$ ) | Air volume ( $\mu\text{L}$ ) | Air flow rate ( $\mu\text{L}/\text{min}$ ) | Duration <sup>a</sup> (s) | Average difference <sup>b</sup> K <sup>+</sup> (%) | Average difference <sup>b</sup> Na <sup>+</sup> (%) |
|----------------------------------|---|------------------------------|--|---------------------------|--|---|
| 250                              | 600   | 250                          | 150  | 150                       | 0.1  | 0.4   |
| 250                              | 600   | 250                          | 300  | 100                       | 1.0  | 2.1   |
| 250                              | 600   | 250                          | 600  | 75                        | 1.6  | 1.9   |
| 250                              | 600   | 250                          | 900  | 67                        | 3.0  | 3.7   |
| 250                              | 600   | 100                          | 600  | 55                        | 12.6   | 10.5  |
| 250                              | 600   | 0 <sup>c</sup>               | 0 <sup>c</sup>                             | 40 <sup>c</sup>           | 25.2   | 25.7  |

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 614 <sup>a</sup> – Duration includes total time for SI elution of DBS and homogenization of the eluate.  
 615 <sup>b</sup> – Difference (%) denotes the difference of analyte's peak area in an eluate, which was  
 616 homogenized by air only, vs. analyte's peak area in the same eluate, which was first  
 617 homogenized by air and subsequently agitated at 1000 rpm for 3 min.  
 618 <sup>c</sup> – Eluate was injected immediately after transfer to the CE vial with no homogenization by air.  
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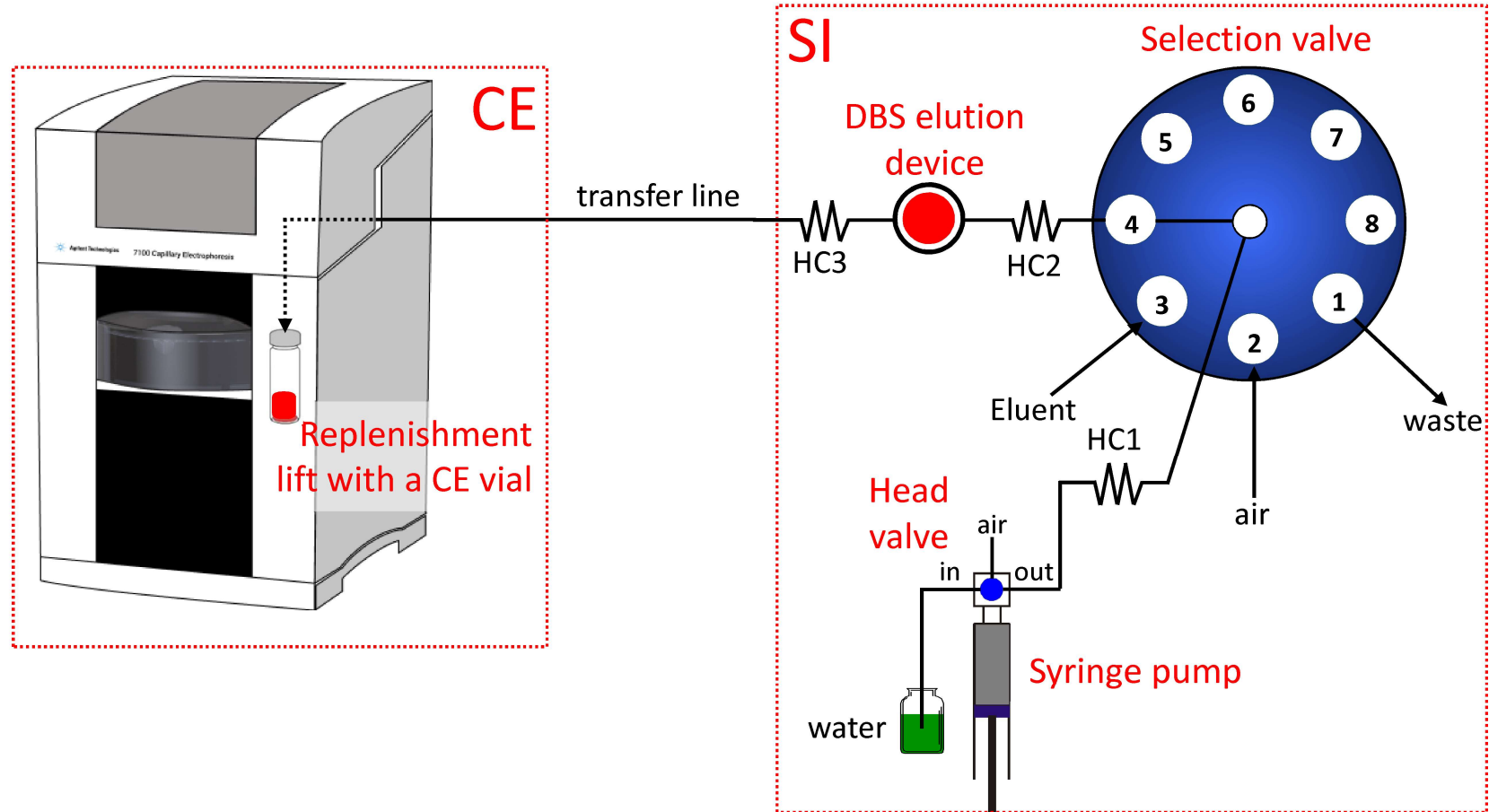
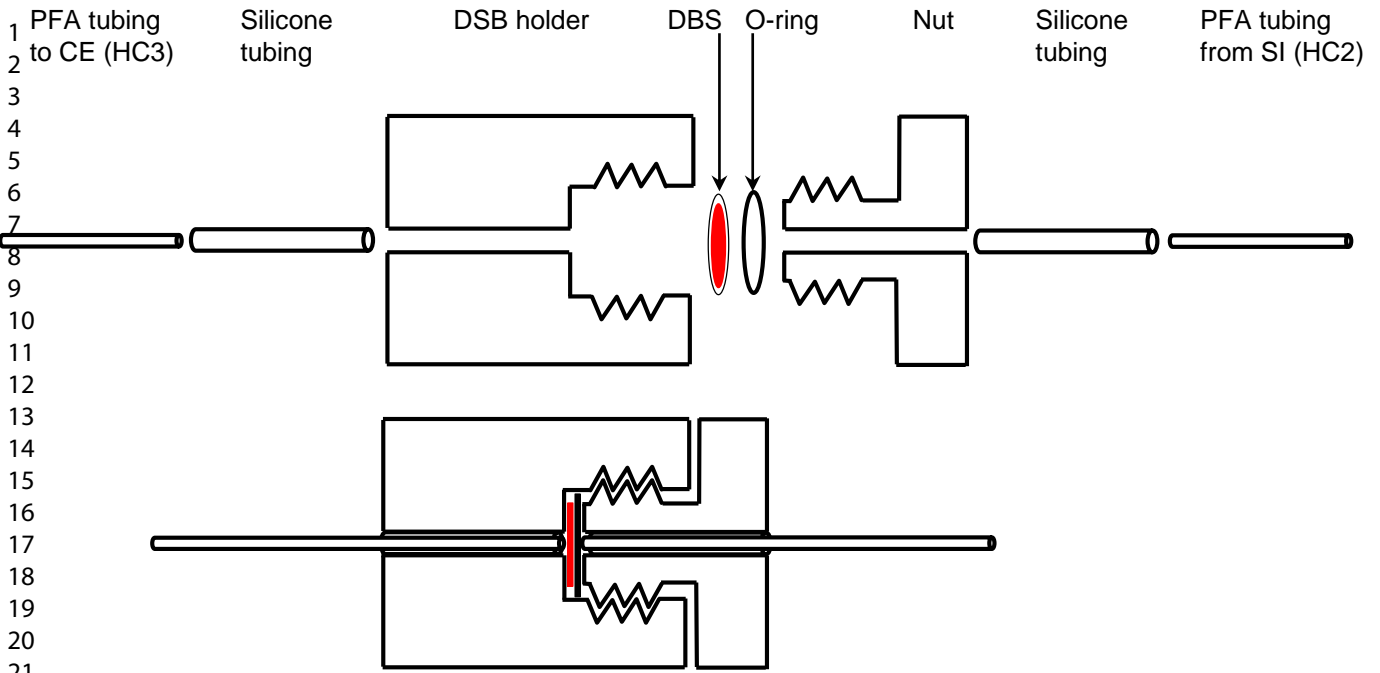


Figure 1



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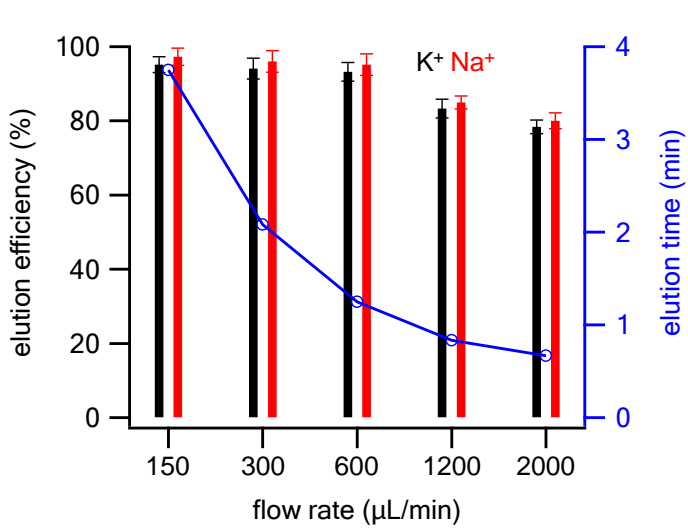


Figure 3

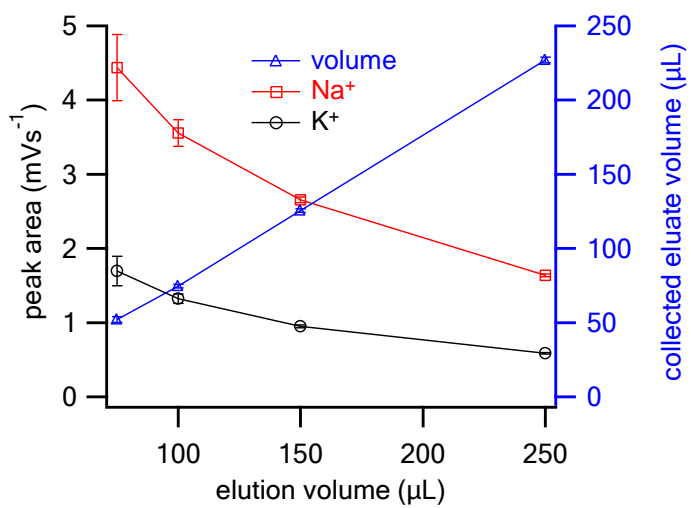


Figure 4



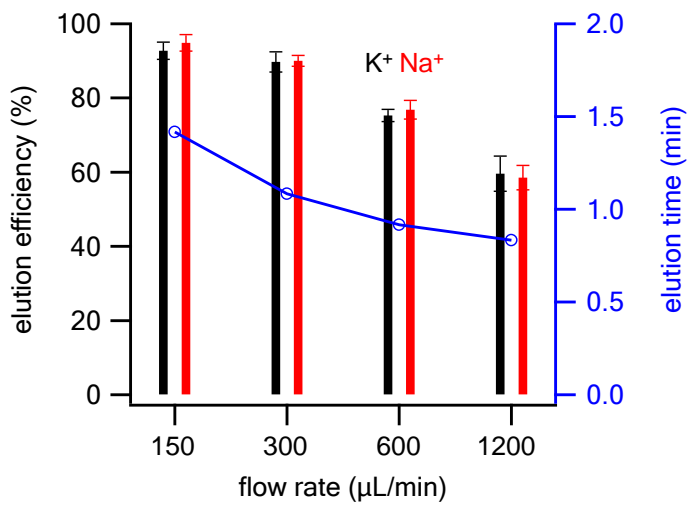


Figure 5

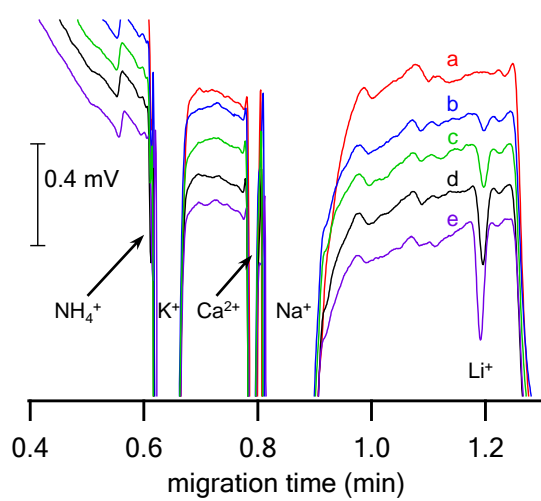
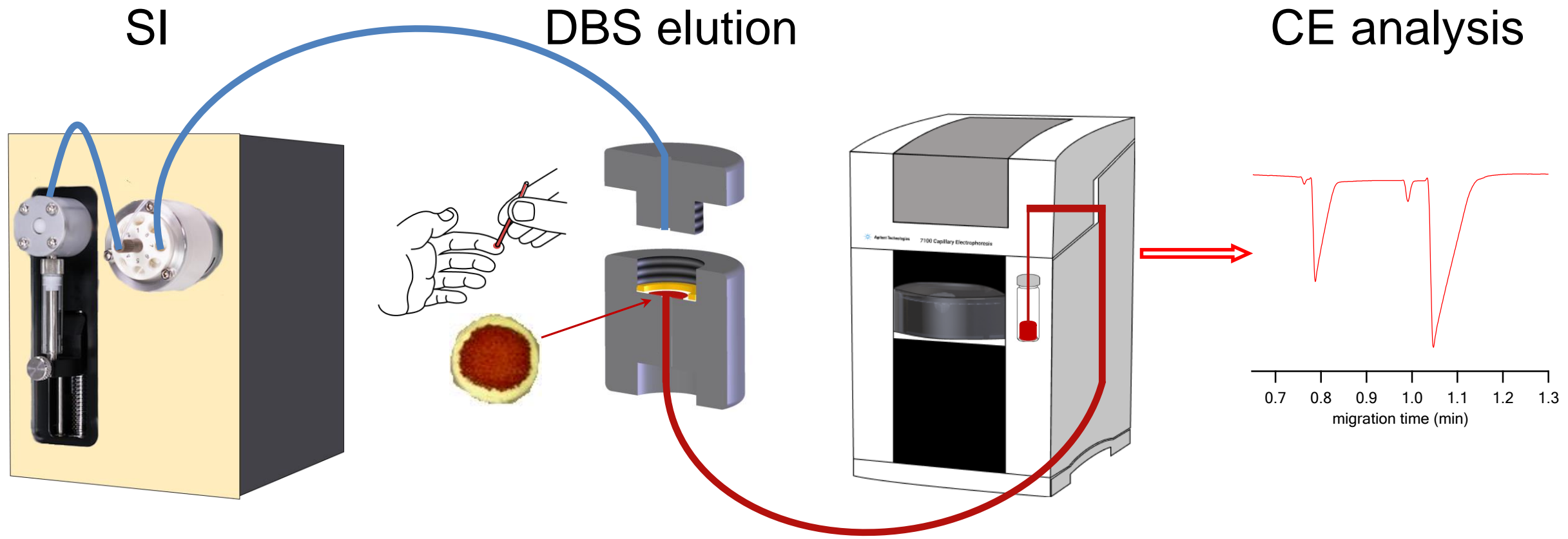


Figure 6



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